

Mars Surface Solar Arrays: Part 2 (Power Performance)



Future In-Space Operations (FISO) Working Group June 7, 2017

NASA

Part 1. Langley Research Center/Richard Pappa Part 2. Glenn Research Center/Tom Kerslake

Outline



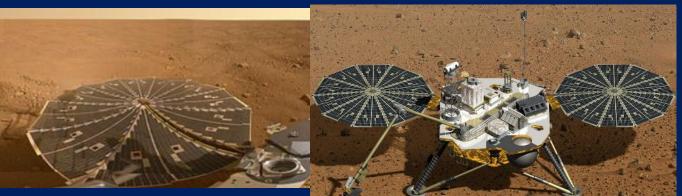
- Heritage solar Mars missions
- Solar Power for a future Human Mars Base
- Mars surface solar fluxes, dust storms
- Solar array configurations, degradation, dust
- "SAWS" conceptual power module
- Daily solar power flow management
- Yearly mission power performance
- Closing comments

Solar Arrays on Mars Right Now



- Robotic missions with flexible power conops
 - Pathfinder (19°N, 1.5m², 0.25 m²/<20 W)
 - MER Spirit & Opportunity (15°S/2°S, 2m², <200 W)
 - Phoenix (68°N, 3m² wings, <150 W)







Human Mars Surface Base Power



- Need continuous day time, night time high power levels
 - Crew/base survival contingency (~5-10 kW?)
 - Effective surface operations (match power availability/usage), 40 kW class
- Limited ability for "safe mode" power downs
 - Sols (for trouble shooting)
 - Months (major dust storm, winter season)
 - So, more onus is on redundancy, system worst case sizing
- Strong desire to demonstrate power capability/margins on Earth during acceptance testing prior to launch
 - Minimize over-sizing (mass penalty) for risk management
 - Known precision landing site, known surface properties
 - Known solar array configuration
 - Engineered/qualified dust abatement/removal
- Emplace & confirm power systems ops before crew launch

Mars Surface Solar Fluxes



- Flux on top of atmosphere (AM0) depends on:
 - Season (Mars Sun distance changes by 18.5%, flux by 38%)
- Total surface flux depends on:
 - Mars season

19°N

- Landing site latitude (sun angles, clear sky & dust storm OD)
 - OD = optical depth (opacity)
- Landing site longitude (local surface albedo)

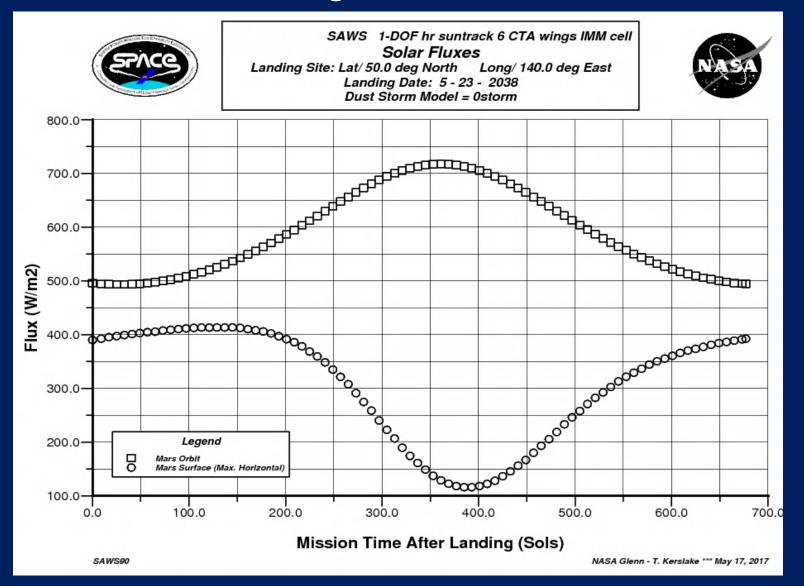
15°S

Dust Storm

Yearly Mars Surface Solar Flux



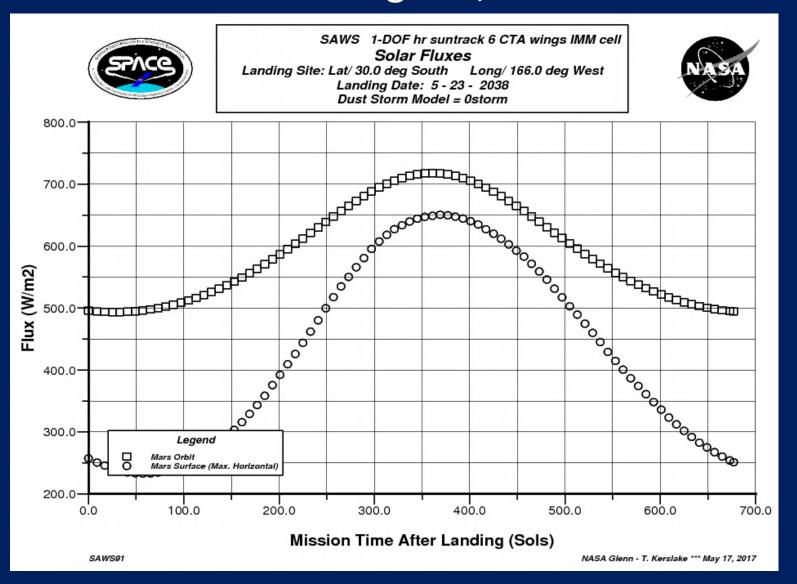
• 50° North latitude landing site, clear skies



Yearly Mars Surface Solar Flux



• 30° South latitude landing site, clear skies

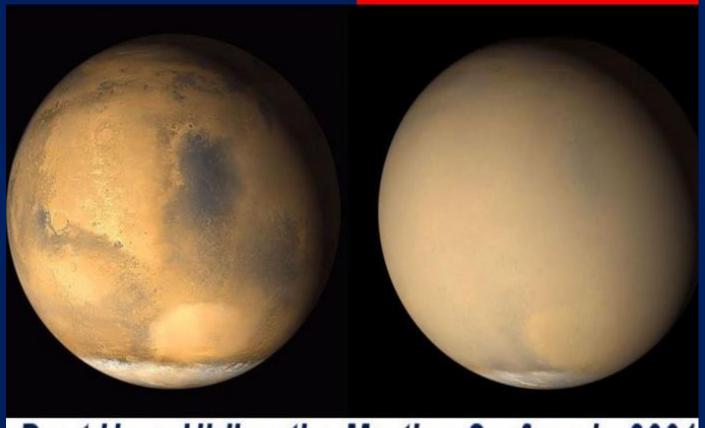


Major (Global) Dust Storms



No Global Dust Storm

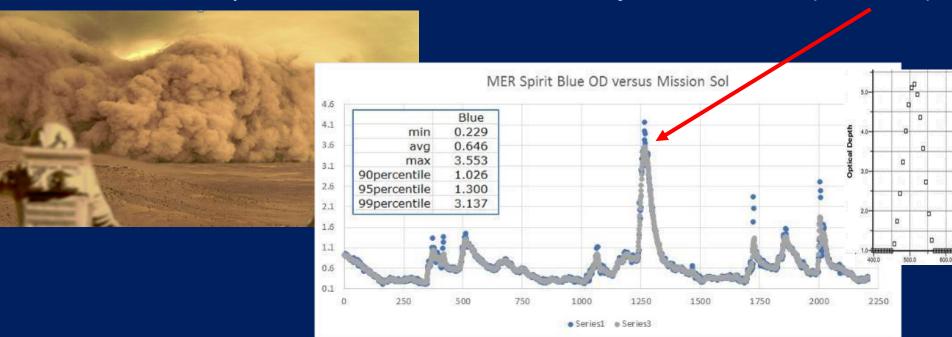
During Dust Storm



Dust Haze Hiding the Martian Surface in 2001

Major Dust Storms - Frequency

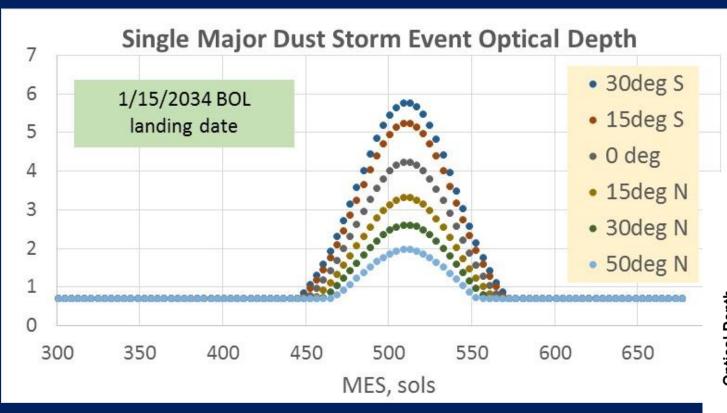
- 0,1,2 major dust storms may occur per Mars year
 - Dust storm covers the globe, 3 month duration, high OD values
 - Occur during summer in the southern hemisphere
 - OD modeled as f(season, latitude, time)
 - Highest OD in the South, lower in the North
 - Historically, ~1/3rd chance each for 0,1,2 major dust storms/yr
 - For these 3 years, MER encountered 1 major dust storm (Jul 2007)



Major Dust Storm OD (Optical Depth)

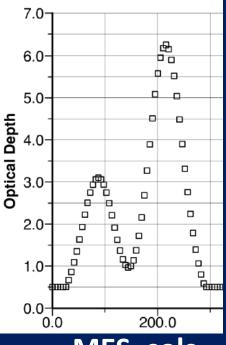


Single storm year OD values



Higher OD values, if a 2nd major storm occurs



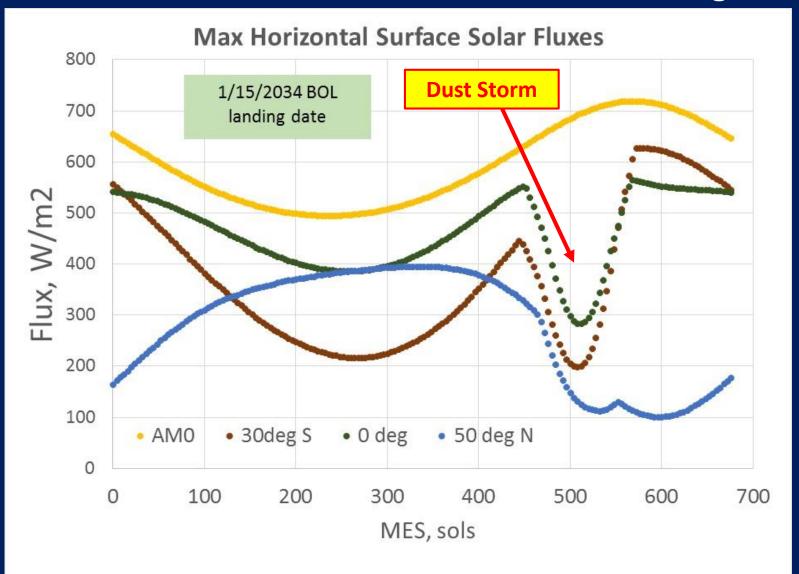


MES, sols

Major Dust Storm Loss in Solar Flux



• From ~30% to 3X reduction in maximum flux – single storm



Mars Surface Solar Flux Components (Important for solar array performance)



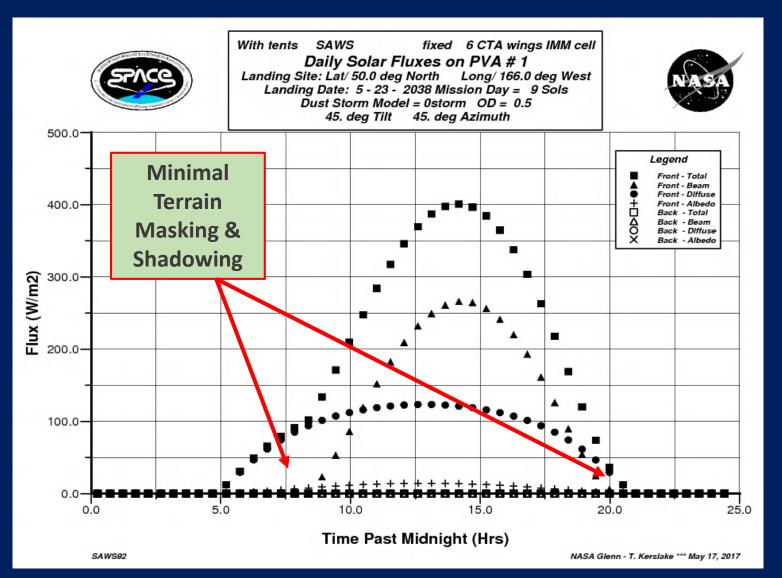
- Total Surface Flux = Beam + Diffuse + Albedo terms
 - Total flux based on net flux function; f(OD,z,al)
 - Directional, spectral forward-back scattering radiation calculation
 - Beam flux based on Beer's Law; f(OD,z,beta)
 - Diffuse flux = Total Beam; f(OD,z,al,theta,beta)
 - Albedo flux based on total irradiance; f(OD,z,al,beta)

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OD = optical depth z = solar zenith angle
al = surface albedo beta = solar array tilt angle
theta = solar array sun incidence angle
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Daily Mars Surface Solar Flux – Clear Skies



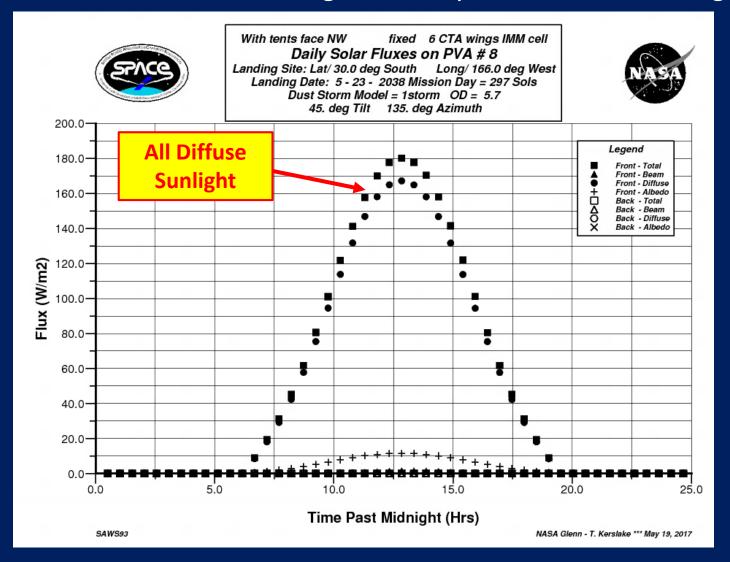
• 45° tilted, fixed South-West facing solar array, 50° North latitude landing site



Daily Mars Surface Solar Flux: At Peak Major Dust Storm OD of ~6



45° tilted, fixed North-West facing solar array, 30°S latitude landing site



Mars Surface Solar Array Configuration



- Must be deployable for high power applications
- Desire planar solar panels
 - Concentrator (8X GCR class) solar arrays less effective (lost diffuse/albedo flux, cleaning optics from dust, substantial tracking losses via uncorrelated errors)
- Fixed horizontal/tilted panels, tracking panels
 - Fixed horizontal panels are simple, little azimuth dependence, maximize power generation for low latitude sites; but lower power at high latitude, highest dust collection rate, passive dust control insufficient
 - Fixed tilted panels (or tents) are simple, can enhance power for high latitude sites, East-West facing panel pairs broaden daily power generation hump, can achieve more strength/stiffness, effective passive dust abatement possible; but have azimuth dependence, reduced power generation (by 20-25%)
 - Tracking panels (typically 1-DOF, N-S or E-W) offer modest power enhancement (5-15%), offer tilting for dust removal / wind load management; but have strong azimuth dependence and mechanisms introduce risk, cost, mass penalties
 - Panels should be kept above the Mars surface ~0.5m to avoid regolith saltation, local string current limiting (possible major/complete loss in power)

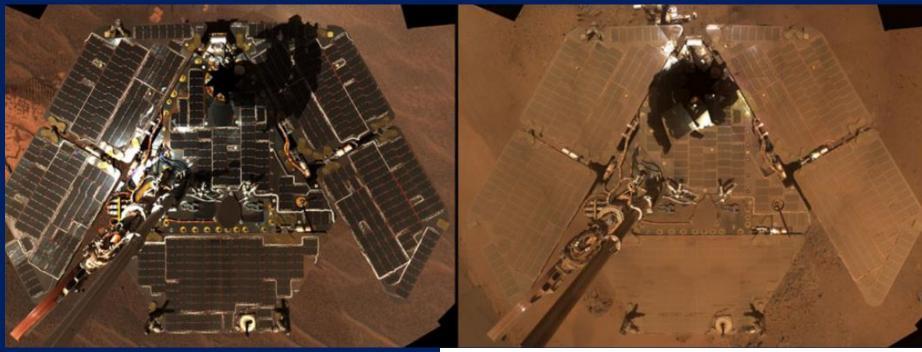
Mars Surface Solar Array Power Degradation Factors



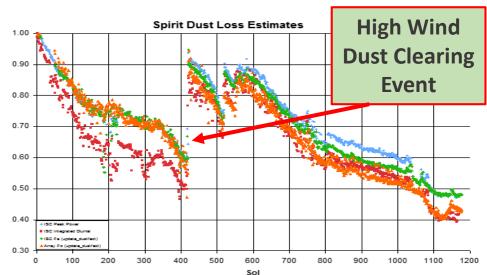
- Even for long missions (6 Mars years), Mars surface environment is mostly benign for solar arrays
 - No concern for proton/electron radiation or GCRs
 - No micro-meteor strike damage
 - Paschen discharge damage eliminated by design
 - Modest thermal cycling, aero-flutter fatigue damage
 - Modest NUV/VUV equivalent sun hours for darkening
 - Modest loss from random failures with proper QTP/ATP
- Dust collection on solar cell coverglass is a major power degradation challenge that must be managed
 - Resident dust blocks sunlight, degrades current output
 - High speed wind blown dust could scratch covers/optical coatings, increase reflectance (degrades current output)
 - Dust could contain corrosive peroxide or perchlorate (need H₂O?)
 - Solar arrays for a high value mission (human life, \$100B's) cannot rely on probabilistic aeolian dust cleaning, i.e. dust devils

MER solar panel dust collection



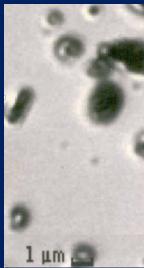


- 0.14% loss per sol
- No power after ~1 year



Dust Management (Abatement, Removal)

- NASA
- Fine dust (micron scale) is an aerosol in the Mars atmosphere constantly precipitating
 - Dust clings via Van der Waals, electrostatic forces
- Human Mars surface base will have many sensitive surfaces (need dust management)
 - Solar arrays, radiators, windows, antennas, lights, nav aides
- "Abatement" avoids dust collection
 - Electrostatic, tilted surfaces
- "Removal" allows dust to collect for periodic removal
 - Piezoelectric shakers, mechanical wipers, electrodynamic, peel-n-discard films, high speed jets (leaf blower, dust devil)
 - Piezoelectric dust removal demonstrated very high effectiveness in ground tests with rigid panels; low mass/power/conops penalties
- Long duration in situ Mars surface demonstration of dust management will be required



Solar Cell Must Operate With Reddened Spectrum



- Mars surface solar fluxes are blue-deplete
 - Function of OD, z (=>landing site, season); MER data below

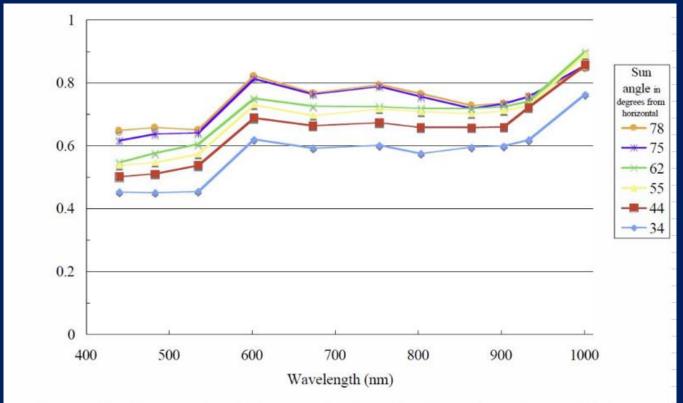
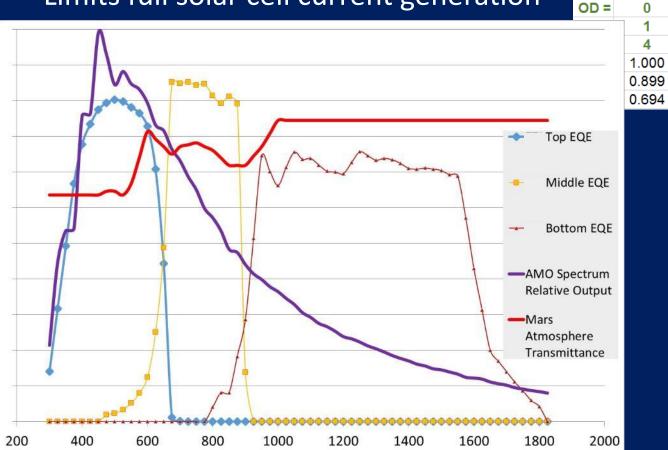


Figure 5: Atmospheric transmission for the global sunlight, 400 nm to 1000 nm, for varied sun angles (averaged for Spirit and Opportunity data, tau approximately 0.94). G. Landis

Solar Cell Spectral Loss on Mars

 Top sub-junction in a high efficiency SOA space multijunction solar cell (using UV/blue wavelengths) will produce less current output than tandem sub-junction

Limits full solar cell current generation



Wavelength, nm

J / IMM4	Cells		
0	0.25	0.5	
1	2	3	
4	5	6	Zen, deg
1.000	0.969	0.944	0
0.899	0.818	0.750	
0.694	0.647	0.608	

Solar Cell Spectral Loss on Mars



- So what to do?
 - Just accept the lost factor, ~10% (for TJ and IMM cells)
 - Size a ~10% larger solar array area (mass, cost increases)
 - Could redesign the cell for better sub-junction current matching (for target OD, z)
 - A tuned "Mars Cell" could recover ~1/2 the loss
 - But a Mars Cell may introduce cost penalties, production challenges, increased risk
 - Could use single junction silicon solar cell
 - Very little spectral loss or even a spectral gain, but ~2X more area needed because of the low conversion efficiency

Mars Surface Solar Array Power Performance Depends on Many Things...

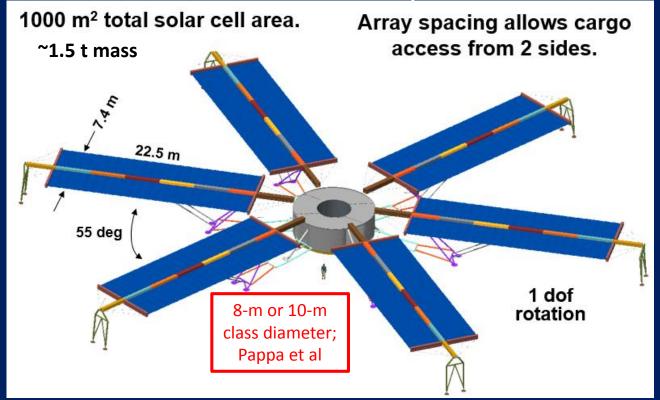


- Mission (most factors covered in prior charts)
 - Date, landing site lat/long, duration, time of day, OD, dust storms
 - Affects solar intensity/spectrum, sun angles, albedo flux, sol day/night periods, environmental temperatures, amount of degradation
- Solar array configuration (in part covered in prior charts)
 - PV cell type, solar cell string length, number & azimuth/tilt angles of solar panels (per design & from surface irregularities), articulation of solar panels
 - Affects solar panel solar flux intensity, shadowing (self, terrain masking) losses, operating temperatures/currents, day time power hump
- Energy storage subsystem
 - Regenerative Fuel Cell (RFC), Battery
 - Affects required solar array size (>50% different), charge rates/periods
- Power management system
 - Voltage regulation (fixed, peak power tracking), day time and night time user load level/profiles, RFC recharge period, power cable lengths (m's or 1 km?)
 - Affects solar panel level operating currents, voltages losses and IV curve operating point

SAWS Module Concept

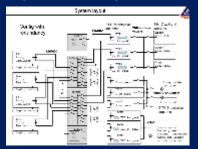


 IMM-populated CTAs, PEM H2/O2 gaseous RFC, 120 VDC regulated PMAD, 10 kW class user power module sizing

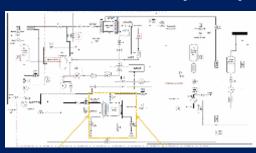


PMAD (1 t class)

RFC (1.9 t)



Araghi & Jakupca



"SAWS" Module Day-Night Power Flow*

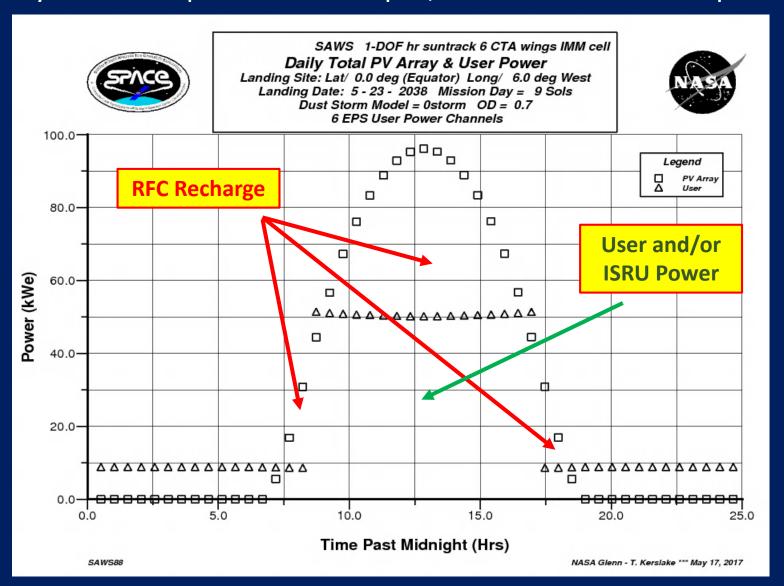


- For Mars base power management conops:
 - Desire near constant user power during the day and the night
 - Managed by base computer and/or crew; Updated week to week and seasonally
 - If ISRU plant is present, it desires constant power for constant ops
- This presents challenges for solar power system
 - Makes power only during the day; power generation has a hump profile
 - Effective day period for user power is shorter than solar day
 - Fuel cell must discharge during the early/late day times when solar array power is low
 - Day faction for day time user power is a selectable parameter
 - Solar power profile changes sol to sol through the mission
 - RFC reactants should be fully used while RFC must be fully recharged sol to sol (nominal ops)
 - So the daily power flow values require an iterative solution for each sol
- Solar power system must be designed for a wide range in daily/yearly power gen operations (mass penalty)
 - Base loads, like ISRU (if present), must also be designed for wide range in power consumption or reduced operating fraction (both, mass penalties)

"SAWS" Day-Night PV, User Power Flow*

NASA

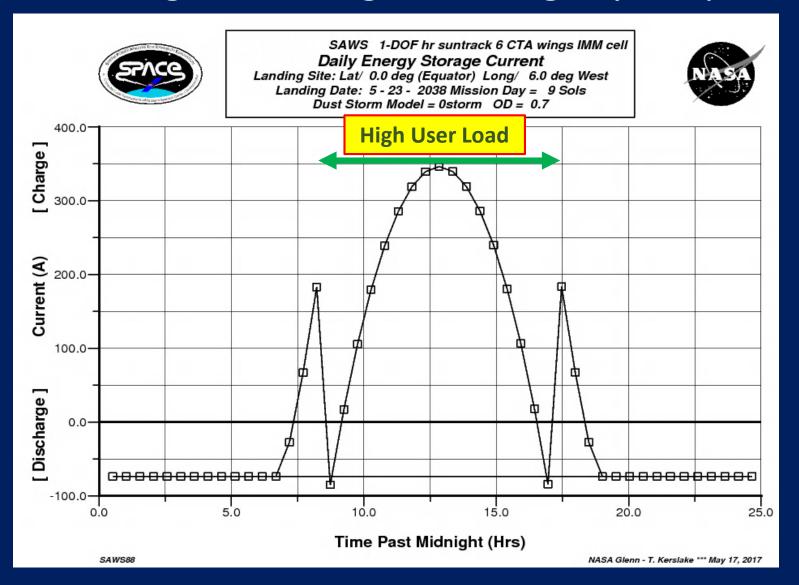
• 60% day time user power factor input, min continuous user power



"SAWS" Module RFC Power Flow*



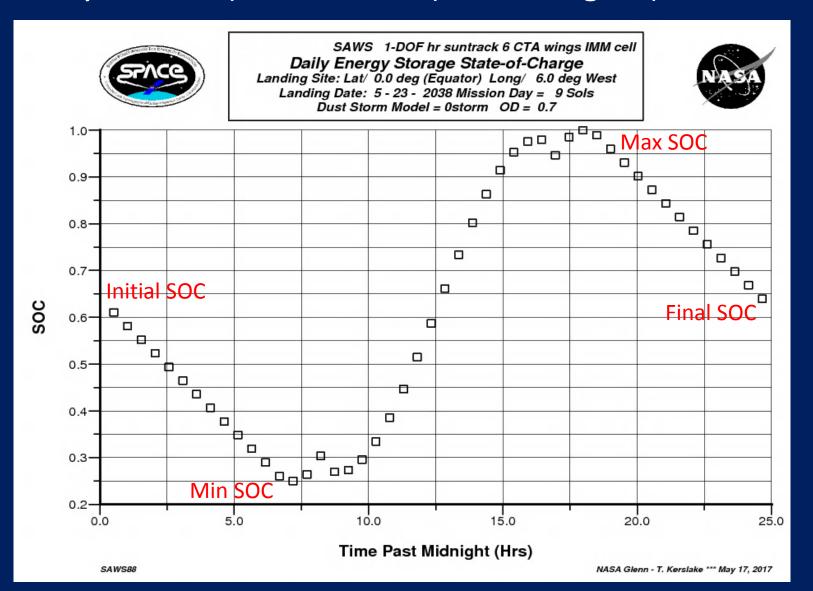
RFC undergoes 3 charge/discharge cycles per sol



"SAWS" RFC Day-Night SOC*



• RFC fully utilized (0.25-1.0 SOC) & recharged (SOCi =SOCf)



"SAWS" Module Mission Power



Equatorial landing site

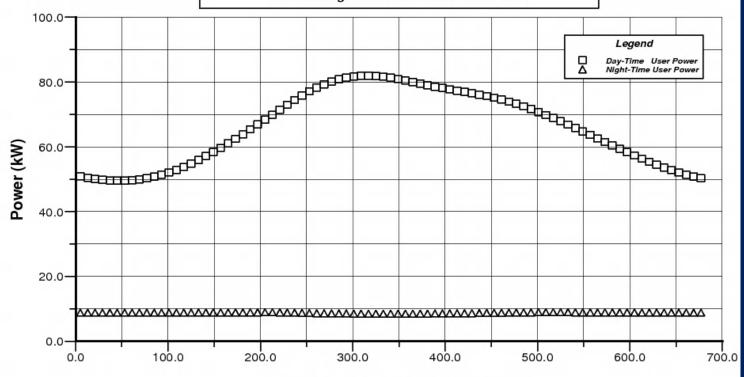


SAWS 1-DOF hr suntrack 6 CTA wings IMM cell
Total User Power

Landing Site: Lat/ 0.0 deg (Equator) Long/ 6.0 deg West Landing Date: 5 - 23 - 2038 Dust Storm Model = 0storm

Total PV Area 996. m2 Total EPS Mass 4.2 MT Sp. Mass (W/kg): PV Panel= 447. PVA= 80. EPS= 8.1 Mission Avg. Total User Power = 29.7 kWe





Mission Time After Landing (Sols)

"SAWS" Module Mission Power



50° North latitude landing site



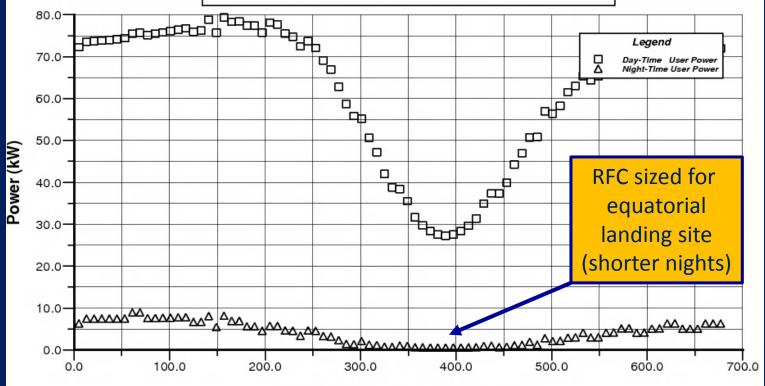
SAWS 1-DOF hr suntrack 6 CTA wings IMM cell
Total User Power

Landing Site: Lat/ 50.0 deg North Long/ 140.0 deg East Landing Date: 5 - 23 - 2038 Dust Storm Model = 0storm

Total PV Area 996. m2 Total EPS Mass 4.2 MT Sp. Mass (W/kg): PV Panel= 447. PVA= 63. EPS= 9.2

Mission Avg. Total User Power = 26.1 kWe





"SAWS" Module Mission Power



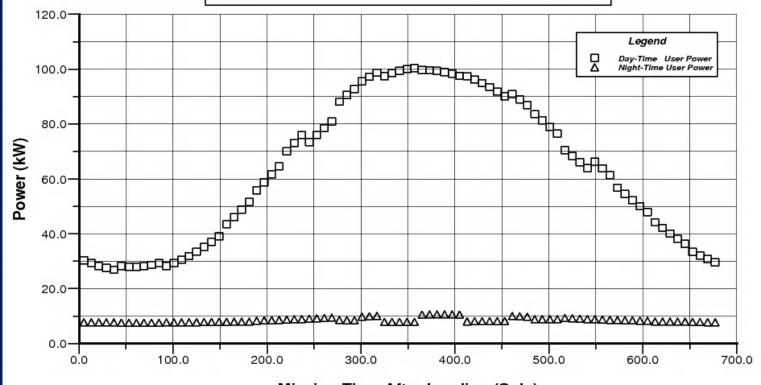
30° South latitude landing site



SAWS 1-DOF hr suntrack 6 CTA wings IMM cell
Total User Power

Landing Site: Lat/ 30.0 deg South Long/ 166.0 deg West
Landing Date: 5 - 23 - 2038
Dust Storm Model = 0storm
Total PV Area 996. m2 Total EPS Mass 4.2 MT
Sp. Mass (W/kg): PV Panel= 447. PVA= 89. EPS= 10.8
Mission Avg. Total User Power = 28.9 kWe





Closing comments



- Solar powered Mars surface human base is feasible
 - Base design and conops will have to reflect solar power system variable power output; equatorial and mid-latitude landing sites only
 - Significant power down required for major dust storm ops
 - The base design and conops will be different from that powered by a fission reactor nuclear power system (i.e., rover/suit recharging, aborts)
 - kW's solar power will be required regardless of primary power system technology choice (nuclear or solar); deployment, emergency power
- Mars surface solar array performance predictions are complex, but amenable to accurate analysis/verification
 - Fortran (type) time-marching, iterating computational analysis tools required
 - Predicts can support system design / component tech-dev planning
 - Simple power estimates have little value (could be >5X in error)

Acknowledgements

- SAWS colleagues across NASA (including LaRC/Richard Pappa)
- NASA GRC/Geoff Landis & Univ. of Tel Aviv/Joe Appelbaum
 - Mars surface solar flux, dust storm modeling; Mars surface solar array data (MER)

Backup material

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Mars surface winds



Wind speed on Mars		R. Pappa	"Feels like" wind speed on Earth (at STP)				
mph m/s d		dynamic pressure	m/s	mph			
		(Pa)					
10	4.5	0.2367	0.6	1.4			
50	22.4	5.9169	3.0	6.8			
67	30.0* +	10.6587	4.1	9.1			
100	44.7	23.6677	6.1	13.5			
150	67.1	53.2523	9.1	20.3			
200	89.4	94.6708	12.1	27.1			
224	100.0	118.4304	13.5	30.3			
447	200.0	473.7216	27.1	60.6			
500	223.5	591.6924	30.3	67.7			

Near surface, horizontal dust devil wind speeds of 75 m/sec (<50 m/sec vertical wind speeds)

+ 2X higher wind speed at 5 m surface elevation up into boundary layer (60 m/sec class)

Highest measured wind speed from Viking Lander (1.6 m sensor elevation) -VL1, sol 209, gusts

SAWS parametric landing sites



Landing sites (site longitude affects albedo solar flux levels)

Parametric		Parametric	Free Choice	
Landing		Pos -> N	Pos -> E	Likely Power
site #	Landing Site Regioanl Name	lat, deg	long, deg	Performance
	Utopia Planitia, very small subsurface			lowest under clear
1	ice depth for ISRU (near VL2)	50	140	skies
2	Mawrth Vallis	30	-20	
3	Jezero Crater (COMPASS study)	19	77	
	Ares Vallis (near Pathfinder,			
4	ExoMars2018)	15	-30	
				medium under clear
5	Meridiani Planum	0	-6	skies; design point
6	Gusev Crater	-15	176	
				highest under clear
				skies; lowest durnig
7	Columbus Crater	-30	-166	major dust storm

Mars surface albedo



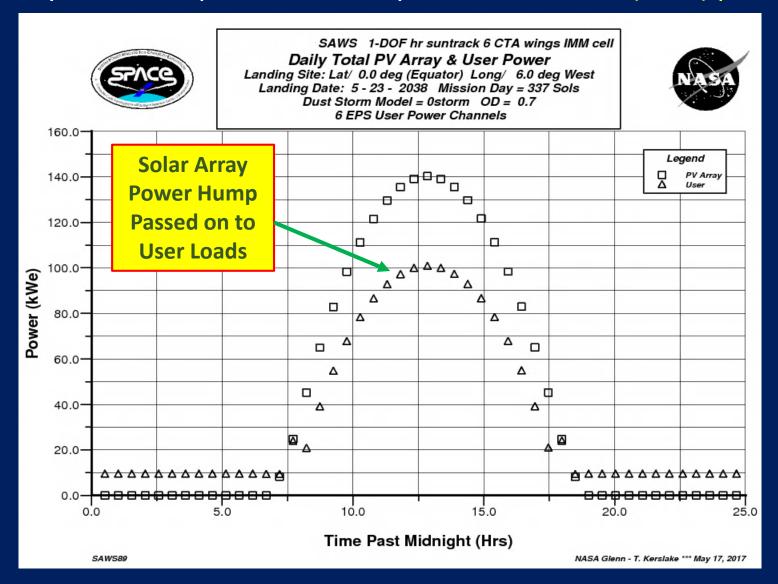
Mars Surface Albedo, 3:1 variation (most important for polar latitude landing sites)

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ongit	ude, de	g								Latitud	le, deg								
st	-90.	-80.	-70.	-60.	-50.	-40.	- 30 .	-20.	-10.	Θ.	10.	20.	30.	40.	50.	60.	70.	80.	9
180.	. 375	. 245	.230	.175	.200	.200	.200	.225	. 255	. 275	.275	.275	.265	.255	.235	.210	.230	. 340	. 4
	.375	.245	.230	175	.200	.200	. 195	.210	.250	.270	.270	.270	.270	.260	.235	.200	.230	. 340	. 4
60.	. 375	.245	.230	.175	.205	.200	. 190	. 195	.240	. 265	.270	.270	.270	.265	.235	.200	.230	. 340	. 4
	. 375	.245	.230	180	.210	.210	. 185	. 180	. 225	. 255	.265	.265	275	.270	.235	.200	.230	. 340	. 4
40.	. 375	.245	.230	. 185	.220	.225	. 185	.175	.200	.250	.260	.260	.275	.270	.235	.210	.235	. 365	. 4
130.	. 375	.245	.230	.185	.225	.230	.190	. 175	. 190	.235	.250	.255	.265	.265	.230	.200	.250	. 425	. 4
20.	. 375	.245	.230	.190	.240	.235	. 195	.175	. 185	.225	.240	.240	.250	.260	.225	. 190	.250	.430	. 4
10.	.375	.245	.230	.190	.240	.235	. 195	. 175	.180	.220	.235	.235	.250	.255	.220	. 185	.250	. 430	. 4
.00.	. 375	.245	.230	. 195	.230	.225	.190	. 175	. 175	.210	.230	.235	.255	.250	.205	. 180	.250	. 430	. 4
90.	. 375	. 245	.230	. 195	.230	.225	.190	. 175	. 175	.200	.225	.230	.250	.248	.190	. 175	.250	. 430	. 4
80.	. 375	.245	.230	.200	.245	.250	.200	. 175	. 170	. 175	.175	,210	.240	.245	.200	. 175	.250	. 430	. 4
70.	. 375	. 245	.230	.200	.250	. 265	.225	. 175	. 160	. 150	. 150	. 185	.230	.248	.210	. 185	. 250	. 430	. 4
60.	. 375	.245	.230	.200	.250	. 265	.225	. 180	.170	. 175	.180	.210	.245	.250	.225	. 190	.250	. 425	. 4
50.	. 400	. 245	.230	. 195	.240	.250	.200	. 180	. 185	.220	.240	.250	.255	.255	.227	. 200	. 235	.400	. 4
40.	. 450	. 259	.230	.190	.225	. 225	. 190	. 180	. 200	. 250	. 265	.270	.260	.250	.230	.210	. 230	. 365	. 4
30.	. 450	. 300	.230	. 185	.215	.220	. 190	. 190	.210	. 250	.275	.275	.265	.250	.230	.210	.230	. 340	. 4
20.	450	. 309	. 230	180	.205	.215	. 195	. 200	. 210	. 245	.270	.275	.265	.250	.230	.210	. 230	. 340	. 4
10.	. 450	. 300	.230	.175	.200	.210	. 195	. 205	. 200	.220	.250	.265	.252	.250	.225	.210	.230	. 340	. 4
-10.	. 450	. 300	.230	.175	.200	.205	. 185	. 182	. 180	.200	.220	.230	.220	.185	.160	. 175	.230	. 340	. 4
-20.	.450	. 300	.230	180	.200	.200	. 180	. 175	. 175	.200	.220	.210	185	.150	.135	. 160	. 230	. 340	. 4
30.	. 450	. 300	.230	.180	.205	.200	. 175	. 170	. 175	.200	.225	.210	.175	.135	.125	. 150	.230	. 340	. 4
40.	. 450	.300	.230	180	.205	.200	.170	. 170	. 175	.210	.230	.225	.185	.150	.135	. 150	.230	. 340	. 4
50.	.400	.250	.230	.180	.205	.200	.175	.170	. 175	. 215	.240	.225	210	.200	.175	. 170	.230	. 340	. 4
60.	. 375	.245	.230	.175	.200	.195	.175	. 175	. 190	. 225	.245	.235	.230	.235	.225	. 190	.230	. 340	. 4
70.	. 375	.245	.230	.175	.190	.195	. 185	. 180	.205	. 250	.260	.255	.255	.265	.250	.210	.230	. 340	. 4
80.	. 375	. 245	.230	.175	.185	.195	. 185	. 180	.215	.270	.285	.277	.277	.275	.255	. 225	.235	. 340	. 4
90.	. 375	. 245	.230	.175	.180	.190	. 185	. 190	. 225	. 285	.300	.285	.280	.275	.262	.230	. 235	. 340	. 4
100.	. 375	.245	.230	.175	.175	.190	.185	.200	.250	.300	.300	.290	.287	.275	.270	.235	.235	. 340	. 4
110.	. 375	.245	.230	.175	.175	.190	.185	.200	.260	, 295	.295	.288	.285	.275	.275	.240	.235	.340	. 4
120.	. 375	.245	.230	.175	.175	.190	.180	.215	.270	.290	.290	.285	.282	.275	.270	.235	.230	.340	. 4
	. 375	.245	.230	.175	.185	.200	.190	.230	.275	.280	.285	.280	.280	.275	.262	. 225	.230	. 340	. 4
40.	. 375	.245	.230	. 175	.195	.200	.200	.240	. 275	.280	.280	.280	.277	.275	.255	. 220	.230	. 340	. 4
150.	. 375	.245	.230	. 175	.200	.200	.200	. 235	.275	. 275	.280	.280	.272	.270	.250	.220	.230	. 340	. 4
.60.	. 375	.245	.230	.175	.200	.200	.200	. 225	.265	. 275	.275	.275	.265	.265	.250	.215	.230	. 340	. 4
L70.	. 375	.245	.230	. 175	.200	.200	.200	. 225	. 260	. 275	. 275	. 275	.265	.260	.240	.210	.230	. 340	. 4
L80.	. 375	.245	.230	.175	.200	.200	.200	.225	.255	. 275	.275	.275	.265	.255	.235	.210	.230	. 340	. 4

"SAWS" Module Day-Night Power Flow



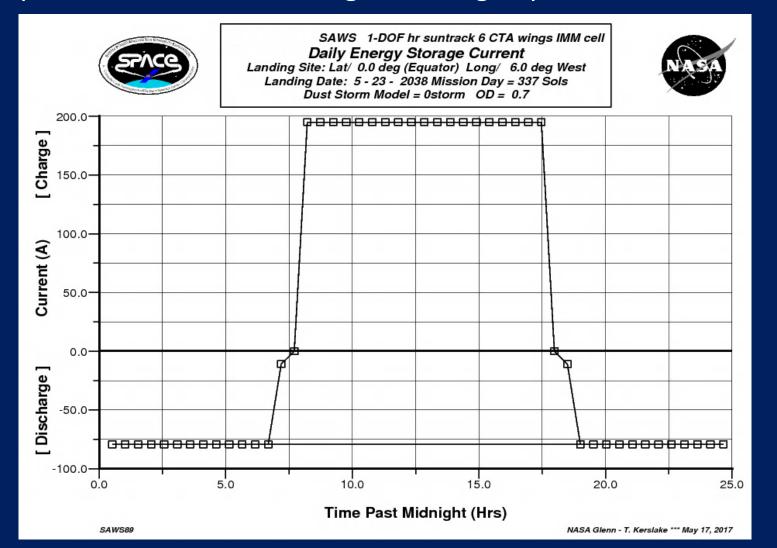
• 60% day time user power factor input, variable user (ISRU) power



"SAWS" RFC Power Flow



- 70% day time user power factor input, variable user (ISRU) power
- Simpler, monotonic RFC charge discharge operation



Mission Day Night Periods





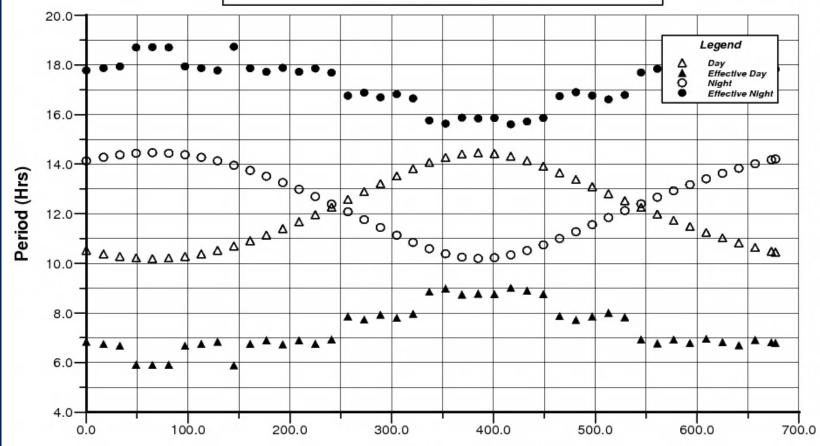
SAWS 1-DOF hr suntrack 6 CTA wings IMM cell

Day & Night Periods

Landing Site: Lat/ 30.0 deg South Long/ 166.0 deg West

Landing Date: 5 - 23 - 2038 Dust Storm Model = 0storm





Mission Time After Landing (Sols)

Mission Environment Temperatures

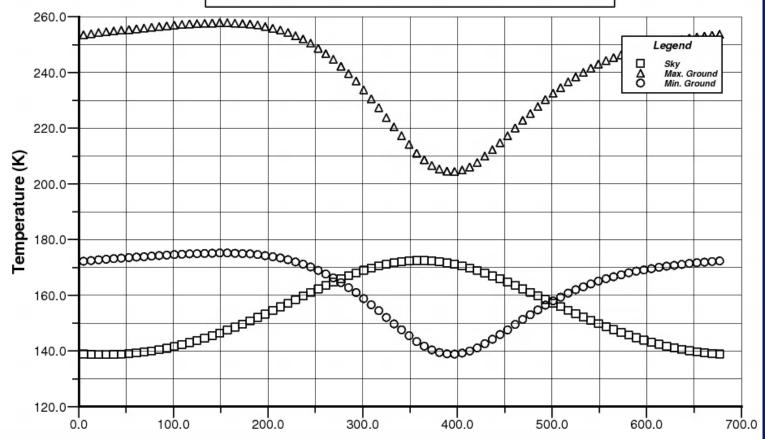




SAWS 1-DOF hr suntrack 6 CTA wings IMM cell Mars Sky & Surface Temperatures

Landing Site: Lat/ 50.0 deg North Long/ 140.0 deg East Landing Date: 5 - 23 - 2038 Dust Storm Model = 0storm





Mission Time After Landing (Sols)

Mission Solar Array Temperatures



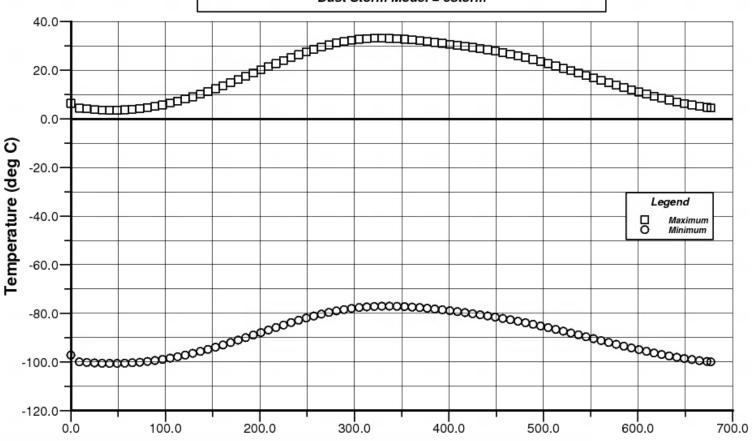


SAWS 1-DOF hr suntrack 6 CTA wings IMM cell PV Wing Temperatures

Landing Site: Lat/ 0.0 deg (Equator) Long/ 6.0 deg West Landing Date: 5 - 23 - 2038

Dust Storm Model = Ostorm





Mission Solar Array Operating Voltage

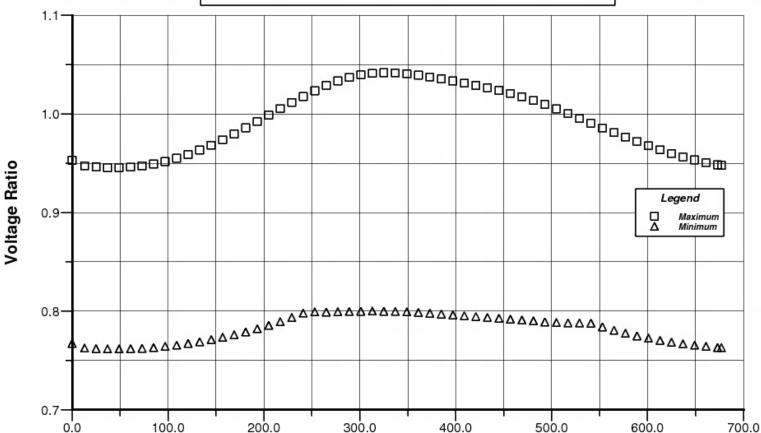




SAWS 1-DOF hr suntrack 6 CTA wings IMM cell Cell Voltage Ratio (Vop/Vmp)

Landing Site: Lat/ 0.0 deg (Equator) Long/ 6.0 deg West
Landing Date: 5 - 23 - 2038
Dust Storm Model = Ostorm





Mission Time After Landing (Sols)